

25 personnel. The tractor's hydraulic power was used to move the protective structure. In order to
26 increase the deployment speed of ROPS, a pressure accumulator was included in the hydraulic
27 circuit. The deployment time of the ROPS without the pressure accumulator was 2.599 s and
28 with the pressure accumulator 0.743 s. The results of the research show that the pressure
29 accumulator assembled in the hydraulic circuit reduced the deployment time of ROPS by 71%;
30 and that the electronic control system can correctly predict overturn. HydraROPS has the
31 advantage compared to other automatic deployment devices of protective structures that can be
32 installed on tractors equipped with a certified rollover protective structure. The installation in
33 marketable tractor models does not modify the protection structure; therefore a new certification
34 of the protection structure is not necessary.

35

36 **Keywords:** Tractor safety; Overturn; ROPS; Injury; Emergency notification.

37

38 **1. Introduction**

39 Tractor overturns are the leading cause of fatalities in the agricultural industry. In USA, nearly
40 50% of tractor fatalities come from tractor overturns (HOSTA, 2004). In Australia, over the
41 2004-07 period, 65 fatalities occurred due to working with tractors, 17 of the deaths (26%) were
42 due to tractor rollover (SWA, 2011). In the EU, a survey carried out by the European
43 Commission of EU member states revealed that 40% of serious injuries and deaths during tractor
44 overturns occurred when a foldable ROPS was not deployed into its protective position (Hoy,
45 2009). In Spain, between 2004 and 2008 the main cause of death in the agriculture sector was the
46 tractor overturning (70%) (Arana et al., 2010). In the Region of Murcia (Spain), over the 2005-
47 2012 period, in 11 of the 44 accidents with tractors, the Roll Over Protective Structure (ROPS)
48 was down at the time when the accident occurred, and this contributed to fatal accidents (Martin-
49 Gorriz et al., 2012). Narrow-track tractors and standard tractors equipped with foldable ROPS

50 are permitted in orchards and vineyards with lowered ROPS. However, due to their complicated
51 ergonomics and the difficulty of handling by the operators, the ROPS tend to remain folded at all
52 times. The consequence is clear; a misuse of the ROPS makes it highly inefficient as a rollover
53 protection system.

54
55 A large number of recent publications are related to applying new technologies and design
56 solutions to promote the automatic deployment of protective structures. Powers et al. (2001)
57 developed an automatically deployable rear-mounted ROPS. It consisted of two subsystems, the
58 first one is a retractable ROPS, which is normally latched in its lowered position for day-to-day
59 use, and the second is a sensor that monitors the operating angle of the tractor. In the event of an
60 overturn, the sensor detects the angle and the retracted ROPS is deployed automatically and
61 locked in the fully upright position before ground contact. This deployable ROPS requires no
62 action to be lifted because it is compressing two springs, located into the fixed part of the ROPS
63 that lift it when two pins that hold the structure in the retracted configuration are simultaneously
64 disengaged by solenoids. Silleli et al. (2007) introduced an additional system for narrow-track
65 orchard and vineyard tractors, developing an automatically deployable telescopic structure which
66 increases the top width of a front-mounted roll bar. The system increased the protection
67 efficiency of the ROPS for the tractor operators and at the same time reduced the overhead
68 clearance required by these machines, to improve potential usage in orchard and vineyard
69 conditions. Ballesteros et al. (2013, 2015) developed and tested an automatically deployable
70 front-mounted ROPS for narrow tractors, using airbag inflators, able to simultaneously increase
71 the height and the upper width of the ROPS. The double change of the ROPS geometry reduces
72 the continuous rolling risk, increases the safety zone in a lateral direction, and allows a reduction
73 in the ROPS height, the bending moments at critical sections, and the ROPS beams sections.

74

75 Other researchers have focused on developing systems capable of informing the tractor operator
76 of the stability of the tractor at all times. Nichol et al. (2005) proposed a device using low-cost
77 sensors and microcomputers to inform the operator of potential tractor instability. DTAEBT
78 (2015) developed an electronic device to monitor tractor stability on sloping ground. Its purpose
79 is to gradually warn the operator as the instability and rollover risk increase. The device called
80 InclSafe can be bought as an aftermarket add-on for a variety of tractor models. Liu and Koc
81 (2013, 2015) developed a smartphone application to transmit the accelerometer and gyroscope
82 signals from a smartphone's built-in sensors to a computer over a wifi network. The application,
83 called SafeDriving, proved how a mobile phone can be used to collect data for the stability
84 assessment of a tractor during operation. These systems try to teach the operator what the risk
85 situations are and what they can do to avoid them.

86
87 The present research sought to develop and test a new automatic system to deploy the ROPS on
88 tractors using hydraulic power; hence this ROPS has been named 'Hydraulic deployment ROPS'
89 (HydraROPS). Two possible options for deploying the ROPS have been considered: (1) the
90 system informs the tractor driver that the stability of the tractor has reached dangerous levels. In
91 the situation above, the driver will be able to use the mechanism to raise the rollover protective
92 bar from the driving seat; and (2) the system automatically deploys the ROPS when the tractor is
93 near to the point of rollover. In this option, it automatically sends a phone message with the GPS
94 location to contact emergency response personnel. This could result in a quicker and more
95 efficient response by emergency personnel, which may in turn save lives or improve the recovery
96 time for non-fatally injured victims.

97

98 **2. Materials and methods**

99 **2.1. Design requirement**

100 HydraROPS is composed of two subsystems: (i) an electronic control subsystem, and (ii) a
101 hydraulic subsystem to move the ROPS. The requirements for the electronic control subsystem
102 were the following:

- 103 • It will be possible to change the ROPS position when the driver recognises a risk
104 situation.
- 105 • Should an immediate rollover condition exists, the ROPS will deploy automatically
106 without the intervention of the driver.
- 107 • Should a potential rollover condition exist, an audible signal will alert the driver.
- 108 • Immediately after a rollover situation, the system will send geographic coordinates of the
109 tractor's location to the emergency call centre.
- 110 • The information related to the movement of the ROPS will be recorded. This data can
111 prove critical in reconstructing the accident. When the ROPS is deployed (manual or
112 automatic mode) time, pitch angle, roll angle and GPS coordinates are recorded. In
113 automatic mode this is recorded plus GPS.

114 The requirements for the hydraulic subsystem were the following:

- 115 • The deployment time of the ROPS will be in time to stop the tractor from rolling onto the
116 driver.
- 117 • The ROPS will remain deployed when the tractor is switched-off.

118 In addition, HydraROPS should be as economical as possible to promote its installation by
119 farmers on their tractors with a front-mounted foldable ROPS.

120 The main advantages of the use of the hydraulic power of the tractor for the deployment of the
121 ROPS are (1) It uses a type of power that exists in all the tractors, and as a part of the tractor
122 circuit is used, this reduces the economic cost of the installation;(2) It can be operated as many
123 times as necessary, (3) It takes up little space and does not interfere with other uses that the
124 farmers give a tractor.

125

126 **2.2. Control algorithm**

127 Tractor overturns are related to various factors, such as a tractor's dimensions, the relative
128 position of the centre of gravity, and dynamics, such as speed, turning radius and terrain. The
129 stability of a tractor can be classified into static and dynamic stabilities. A stability index based
130 on static stability is simple, thus it is more easily applied as the first step to automatic
131 intervention in an engineering control. In this research, the mathematical model proposed by Liu
132 and Ayers (1998) was used. The authors proposed the development of a stability index in a
133 combination of pitch and roll (SI_{COM}). Their work showed that the stability indices indeed
134 predicted instability at the times of overturn for both side and rear overturn. The details of this
135 control algorithm can be found in Liu and Ayers (1998). The overall stability index value was
136 calculated using the following equation (1):

137

$$138 \quad SI_{COM} = \left[1 - \sqrt{\left(\frac{\theta^2}{\theta_{cri}^2} + \frac{\phi^2}{\phi_{cri}^2} \right)} \right] \times 100 \quad (1)$$

139

140 where θ and ϕ are the pitch angle and roll angle of the vehicle and θ_{cri} and ϕ_{cri} are the critical
141 pitch angle and critical roll angle, at which lateral or longitudinal overturning is about to happen.
142 The stability index (SI_{COM}) values range between 0 (least stable) and 100 (most stable). The
143 algorithm for activating deployment of a safety system proposed by Liu and Ayers (1998) was
144 the following criteria (2):

$$145 \quad SI_{COM} \leq SI_{cri} = 0 \quad (2)$$

146

147 **2.3. Electronic control subsystem**

148 The electronic control subsystem was designed for two modes of operation (Fig. 1): mode 1,
149 voluntary operation by the tractor driver, and mode 2, automatic operation in the event of
150 imminent roll over. The software uses the physical parameters of the tractor and the data from
151 the sensors of the electronic subsystem to conduct the signal processing and implementation of
152 the control algorithm. Two warning levels were defined. In the first level, when the stability
153 index (SI_{COM}) value was below 40, an audible warning signal was switched on, and the second
154 level, when the SI_{COM} value was below than 20, the ROPS was deployed.

155

156 [Figure 1. insert here].

157

158 The electronic control subsystem which acts on the hydraulic circuit was based on a
159 microcontroller board with other components. Fig. 2 shows the system architecture of the
160 HydraROPS prototype. The components that were used in the electronic control subsystem were
161 the following:

162 1. **Microcontroller circuit.** An Arduino ATmega2560 microcontroller board was used that
163 has a number of I/O ports suitable for the electronic components used. The assembly of
164 the components was modular. The software was programmed in the C language. Fig. 3
165 shows the flowchart for the algorithm used by the microcontroller.

166 2. **Inertial measurement unit.** An inertial measurement unit (PMU6050) composed of an
167 accelerometer and a gyroscope was used. This device senses static and dynamic
168 accelerations and computes the angle at which the tractor is operating. A Kalman filter
169 was used to filter the noise from the accelerometer and gyroscope sensors. The Kalman
170 filter is a set of mathematical equations that provide an optimal means of estimating the
171 state of a process so that the error is minimised. This filter is widely used in navigation
172 and control systems.

- 173 3. **Communication module.** The communication module SIM908 was used to connect
174 GSM network and receive GPS. This shield with a Quad-band GSM/GPRS engine works
175 on frequencies EGSM 900MHz/DCS 1800MHz and GSM850 MHz/PCS 1900MHz. It
176 also supports GPS technology for satellite navigation. The combination of both
177 technologies allows goods, vehicles and people to be tracked seamlessly at any location
178 and at any time with signal coverage. When the device operates automatically (mode 2)
179 the GSM/GPRS module was activated and sends a short message (SMS) with the
180 geographic coordinates of the tractor's location. This could result in a quicker and more
181 efficient response by emergency personnel, which may save lives or improve the
182 recovery time for non-fatally injured victims.
- 183 4. **Memory card.** The microSD memory card (Arduino microSD shield) was used to record
184 the data. When HydraROPS was moved manually or automatically the following data
185 were recorded in the memory card: time (hh:mm:ss), pitch angle (degrees), roll angle
186 (degrees), geographic coordinates (longitude and latitude), position of the ROPS
187 (horizontal or vertical position) and mode to switch-on the ROPS (mode 1 or 2).
- 188 5. **Relay module.** In the full-scale tractor the relay module was used to operate the
189 hydraulic subsystem. The normally open contacts of the relay were connected to solenoid
190 valves that, when ignited, deploy the hydraulic cylinders of the HydraROPS. Solid-state
191 relays were used because they are more robust than electromechanical relays. In the scale
192 model tractor a solenoid coil was used to deploy the ROPS.

193
194 These electronic components were placed inside a box panel with IP (International Protection)
195 code 66. The box panel was located close to the steering wheel of the tractor to make it easily
196 accessible for the tractor driver, because in mode 1 the ROPS is switched on by the driver.

197

198 [Figure 2. insert here].

199

200 [Figure 3. insert here].

201

202 **2.4. Hydraulic subsystem**

203 HydraROPS was designed to be mounted on a tractor with a front-mounted deployable ROPS.

204 Fig. 4 shows the hydraulic circuit of HydraROPS. In order to make the prototype less expensive,

205 the hydraulic power of the tractor was used to move the deployable ROPS (Carraro, X 260-3).

206 Two hydraulic cylinders, (CHB 50/30 – 150, stroke length of 150 mm, bore diameter of 50 mm,

207 piston rod diameter of 30 mm and maximum operating pressure of 20 MPa) one on each side of

208 the ROPS, raised and lowered the structure. In a preliminary study, it should be noted that

209 deployment time was evaluated in comparison to other power sources such as spring action

210 technology (Powers et al., 2001) or airbag inflators technology (Ballesteros et al., 2013). In order

211 to solve this problem, a bladder pressure accumulator was included in the hydraulic circuit for

212 faster deployment of the ROPS. In addition, the pressure accumulator (volume of 1.5 L and

213 pressure of 7 MPa, Hydro Leduc, Azerailles, France) allows a last activation of the ROPS even

214 though the tractor engine has been switched off.

215

216 [Figure 4. insert here].

217

218 **2.5. Economic assessment**

219 Figure 5 shows hydraulic and electronic components of HydraROPS installed in a Case 2120V

220 tractor with a certified protection structure. Figure 6 shows this tractor with ROPS in retracted

221 position and in deployed position. The total cost to place the HydraROPS in this tractor was

222 2176 €. Hydraulic components were the highest item totalling 1016 € (47 %), followed by the

223 electronic components at 522 € (24 %). The cost of the labour to assemble the electronic and
224 hydraulic components was 636 € (29 %). The cost reported here was for a prototype device. The
225 device is not yet marketable. This cost can no doubt be reduced with large scale quantities. In the
226 not too distant future, we aim to sell HydraROPS as a kit for marketable tractor models with a
227 front-mounted deployable ROPS.

228

229 [Figure 5. insert here].

230

231 [Figure 6. insert here].

232

233 **3. Performance evaluation**

234 **3.1. Electronic device test in scale tractor**

235 The evaluation of the electronic devices was made in a scale (1:16) remote-control tractor
236 implemented with the electronic components of the prototype. The track width of the scale
237 tractor was 127 mm, the height of the centre of gravity was 66 mm, and the mass of the scale
238 tractor with the electronic components was 1062.2 g. The critical roll and critical pitch angles
239 values were calculated for the control algorithm. These physical parameters of the tractor and the
240 data from the sensors were used for implementation of the control algorithm. Fig. 7a shows the
241 scale tractor with ROPS in the operating position. The Solid Works v. 2012 (SolidWorks Corp.,
242 Massachusetts, USA) computer program was used to design a three-dimensional (3D) model of
243 the ROPS. The ROPS was built in acrylonitrile butadiene styrene using a 3D printer (Dimension
244 BST 1200ES). The dimensions of the ROPS to the protection of the clearance zone for the driver
245 have been calculated according to OECD Code 6 (2012). A solenoid coil was used to activate the
246 spring that was deployed the ROPS. The scale tractor was operated on a test platform with a
247 rising slope in laboratory conditions (Fig. 7b). The test platform has ascending and descending

248 slopes, and also side slopes to test the scale tractor under different conditions. The measured and
249 calculated data were transmitted to a personal computer via USB connection for further analysis
250 and reporting.

251

252 [Figure 7. insert here].

253

254 **3.2. Deployment time of HydraROPS test**

255 A high speed camera (Faster Imaging Trouble Shooter TSHRMS, Artisan Technology Group,
256 Champaign, IL, USA) was used to determine the time required to extend the structure. The
257 hydraulic circuit of HydraROPS (Fig. 4) was installed in a Case tractor model 2120V that was
258 used for this test. The tests were run in two sets of five deployments, five of them with the
259 pressure accumulator disassembled and five of them with the pressure accumulator assembled.
260 The deployment time was measured with the tractor at engine speed of 989 rev min⁻¹. Data were
261 analysed by one-way ANOVA, and differences among means were determined with Fisher's
262 (LSD) Multiple-Range Test using Statgraphics Plus, version 5.1., STSC Inc., Rockville, MD,
263 (USA). All significant differences were determined at the 0.05 level of significance.

264

265 **3.3. Electronic device test in real tractor**

266 After testing the electronic device subsystem in the scale tractor, HydraROPS was then tested on
267 a Case 2120V tractor. Field upset tests were conducted at the Agricultural Experimental Station
268 of the Technical University of Cartagena. The path was 114 m with a maximum pitch angle of
269 33.59° and maximum roll angle of 25.65°.

270

271 **4. Results and discussion**

272 **4.1. Electronic device test in scale tractor**

273 Several factors were considered when deciding to build a scale safe tractor. The first one was to
274 verify the correct operation of the electronic control subsystem, whilst the second one was its use
275 for teaching tractor safety in an Open Day for secondary school children at the Technical
276 University of Cartagena. The scale tractor has been used to teach basic knowledge such as:
277 explaining the role that the centre of gravity plays in tractor overturns or explaining how to be
278 protected during a tractor overturn.

279

280 **4.2. Hydraulic circuit tests**

281 Table 1 shows the deployment time of HydraROPS in the Case 2120V tractor with the pressure
282 accumulator disassembled and assembled. In our experimental conditions, when the pressure
283 accumulator was assembled in the hydraulic circuit, the deployment time was reduced by 71%.
284 This result shows it is necessary to include a pressure accumulator in the hydraulic circuit, when
285 hydraulic power is used to move the ROPS.

286

287 [Table 1. insert here].

288

289 A large reduction of the deployment time (71%) was produced by the use of the pressure
290 accumulator in the hydraulic circuit of HydraROPS. However, with other technologies the time
291 to extend the ROPS was less than with our prototype. In this sense, the spring-type system
292 developed by Etherton et al. (2002) deployed the structure in 0.202 s, the telescopic structure
293 developed by Silleli et al. (2008) deployed the structure in 0.160 s, and the airbag inflators
294 system developed by Ballesteros et al. (2015) deployed the structure in 0.312 s. Therefore, we
295 are working on a new hydraulic circuit to further reduce the deployment time of HydraROPS.

296

297 It should be noted that the literature offers findings about the overturning duration, which is
298 0.750 s according to Hathaway and Kuhar (1994) or 0.720 s according to Silleli et al. (2008).
299 This time was approximately the same as the time required to deploy the HydraROPS prototype.
300 In addition, by software it is possible to modify the stability index value to automatically start the
301 deployment the HydraROPS with less slope, and thus save time.

302

303 **4.3. Electronic device test in real tractor**

304 Fig. 8 shows pitch angle and stability index in a rearward upset field test, and Fig. 9 shows roll
305 angle and stability index in a sideward upset field test. The criterion that has been used for
306 deployment of ROPS following the Eq. (1) was that when the pitch angle or roll angle or both
307 are above the critical angle value the deployment of ROPS was activated. The experimental
308 results showed that the ROPS was deployed at 102 s from the start of the route. In this time the
309 combination of pitch angle (23.48 degrees) and roll angle (13.25 degrees) produced a stability
310 index value below 20.

311

312 [Figure 8. insert here].

313 [Figure 9. insert here].

314

315 **5. Conclusions**

316 A hydraulic deploying mechanism for ROPS has been designed, constructed and tested to be
317 used for agricultural tractors with a front-mounted ROPS. The deployment time of the
318 mechanism was tested using an existing tractor ROPS. The results of the research show that the
319 pressure accumulator assembled in the hydraulic circuit reduced the deployment time of ROPS
320 by 71%. The deployment time was 0.743 s. The electronic control system can correctly predict
321 overturn; in automatic mode, when the stability index value was below 40, an audible warning

322 signal was switched on, and when the stability index value was below 20, the ROPS was
323 deployed. The system sent geographic coordinates of the tractor's location to the emergency call
324 centre, and information related to the movement of the ROPS will be recorded. This data can
325 prove critical in reconstructing the accident.

326
327 HydraROPS has been patented (Ibarra Berrocal et al., 2015) and it has the advantage compared
328 to other automatic deployment devices of protective structures that it can be installed on tractors
329 equipped with certified rollover protective structures. The installation of HydraROPS in a tractor
330 does not modify the protection structure, therefore a new certification of the protection structure
331 is not necessary.

332
333 The results reported here are for a prototype device. The device is not yet marketable. Current
334 plans are to continue developing HydraROPS employing a new hydraulic circuit to further
335 reduce the deployment time of ROPS, and improve the control algorithm using the dynamic
336 stability index developed by Liu and Ayers (1999).

337
338 **Acknowledgements**
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340 “new safety devices in machinery”.

341
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410

411 **Tables and Figure Captions**

412 **Table 1.** Deployment time of HydraROPS in Case 2120V tractor.

413

414 **Figure 1.** Schematic diagram of the two possible modes to switch on HydraROPS.

415 **Figure 2.** System architecture of HydraROPS.

416 **Figure 3.** Flowchart for the algorithm used by the microcontroller.

417 **Figure 4.** Hydraulic circuit of HydraROPS.

418 **Figure 5.** Hydraulic and electronic components of HydraROPS installed in a Case 2120V
419 tractor. (a) hand box panel, (b) electronic box, (c) hydraulic cylinder, (d) electro-hydraulic circuit
420 of HydraROPS, (e) pressure accumulator, (f) exterior protection.

421 **Figure 6.** Case 2120V tractor with HydraROPS prototype installed. (a) ROPS in retracted
422 position (b) ROPS in deployed position.

423 **Figure 7.** (a) scale tractor, (b) test platform.

424 **Figure 8.** Pitch angle and stability index in a rearward upset field test.

425 **Figure 9.** Roll angle and stability index in a sideward upset field test.

426

427

Table 1. Deployment time of HydraROPS in Case 2120V tractor.

Type of test	Time (s)	
	Average value recorded of the 5 tests	Maximum value recorded of the 5 tests
Pressure accumulator disassembled	2.575 a	2.599
Pressure accumulator assembled	0.733 b	0.743

Treatments with different letters had significant differences according to Fisher (LSD) at 95.0%.

Figure 1

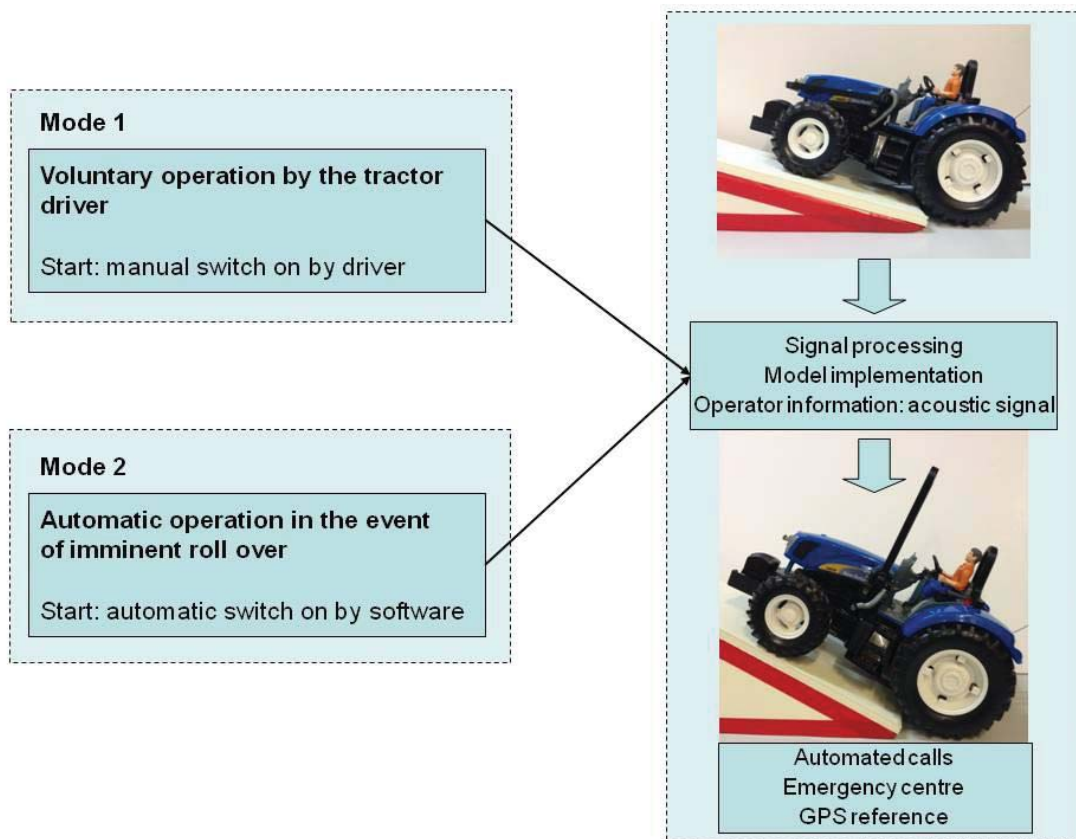


Figure 1. Schematic diagram of the two possible modes to switch on HydraROPS.

Figure 2

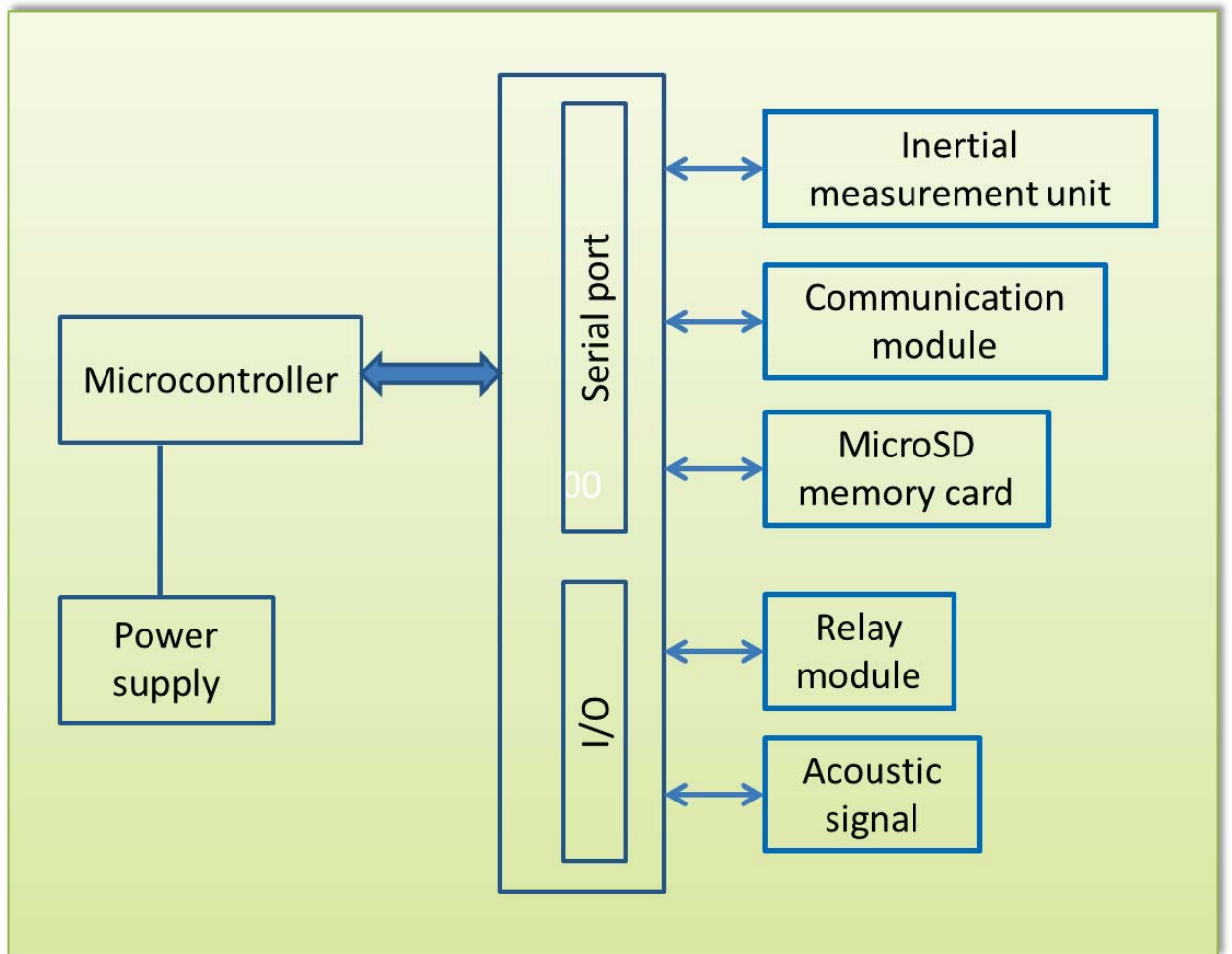


Figure 2. System architecture of HydraROPS.

Figure 3

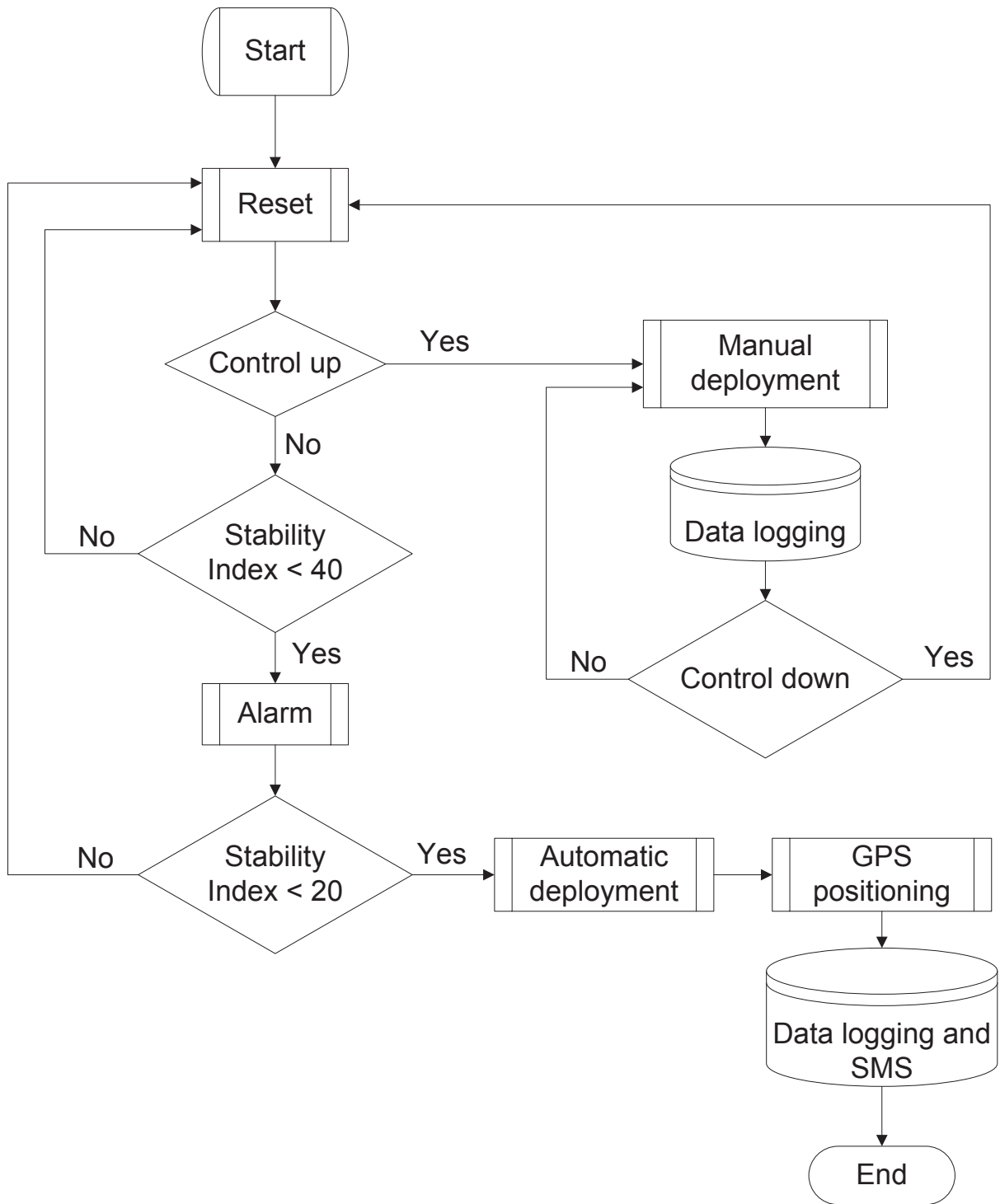


Figure 3. Flowchart for the algorithm used by the microcontroller.

Figure 4

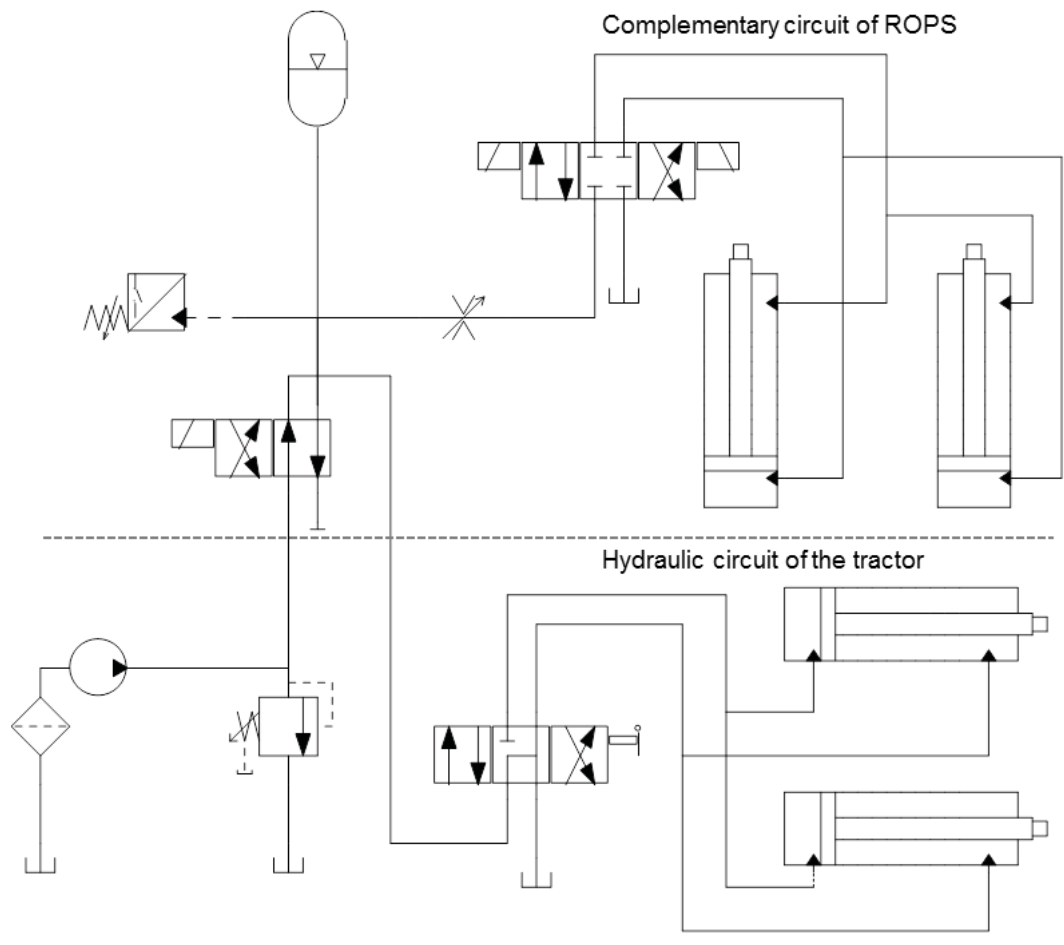


Figure 4. Hydraulic circuit of HydraROPS.

Figure 5

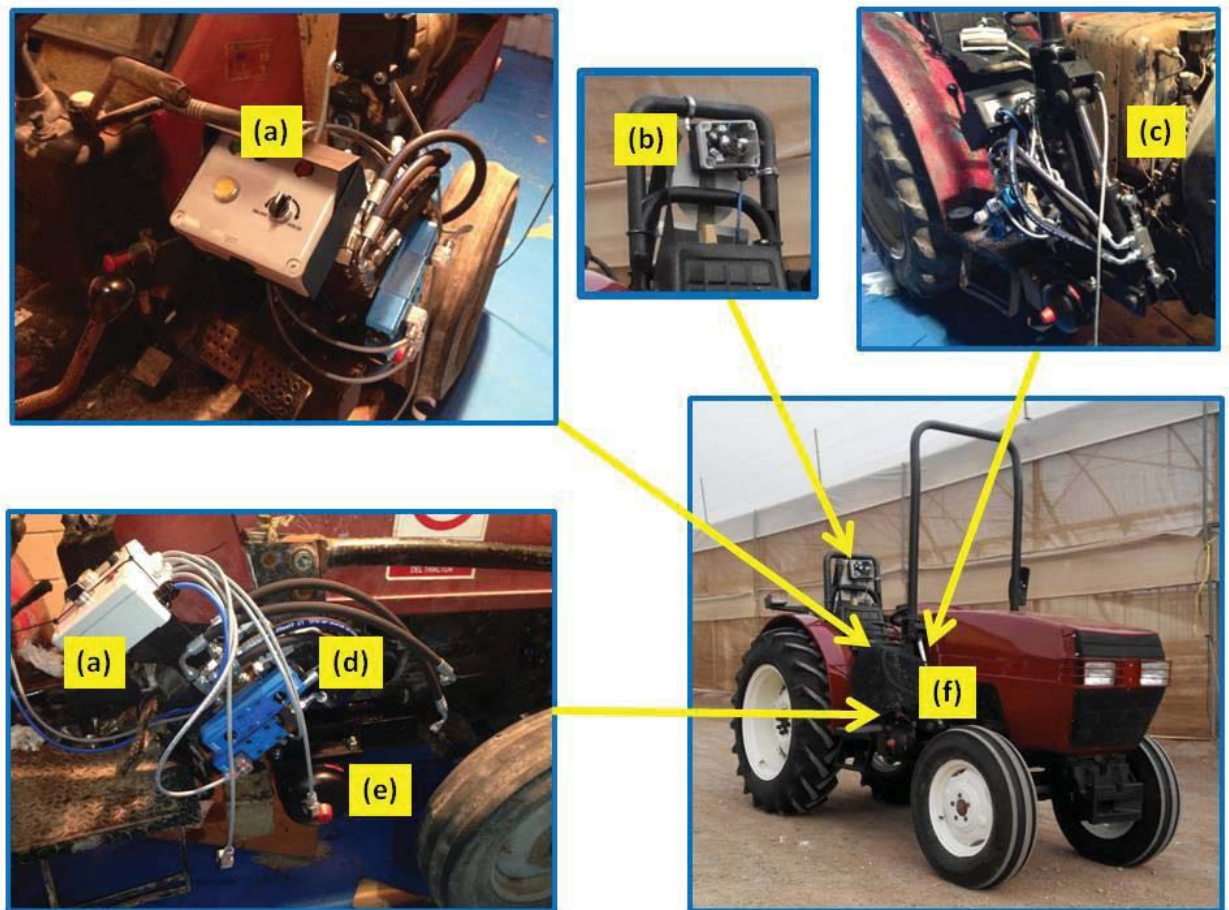


Figure 5. Hydraulic and electronic components of HydraROPS installed in a Case 2120V tractor. (a) hand box panel, (b) electronic box, (c) hydraulic cylinder, (d) electro-hydraulic circuit of HydraROPS, (e) pressure accumulator, (f) exterior protection.

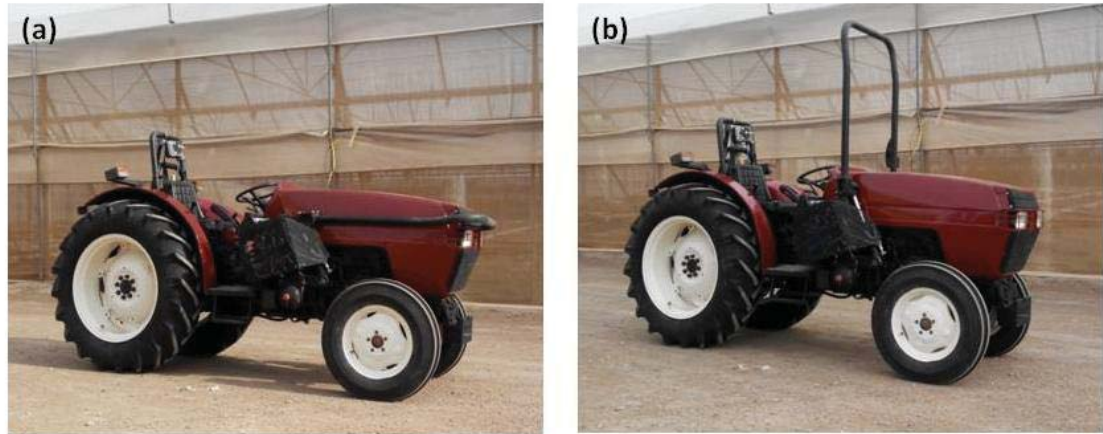


Figure 6. Case 2120V tractor with HydraROPS prototype installed. (a) ROPS in retracted position (b) ROPS in deployed position.

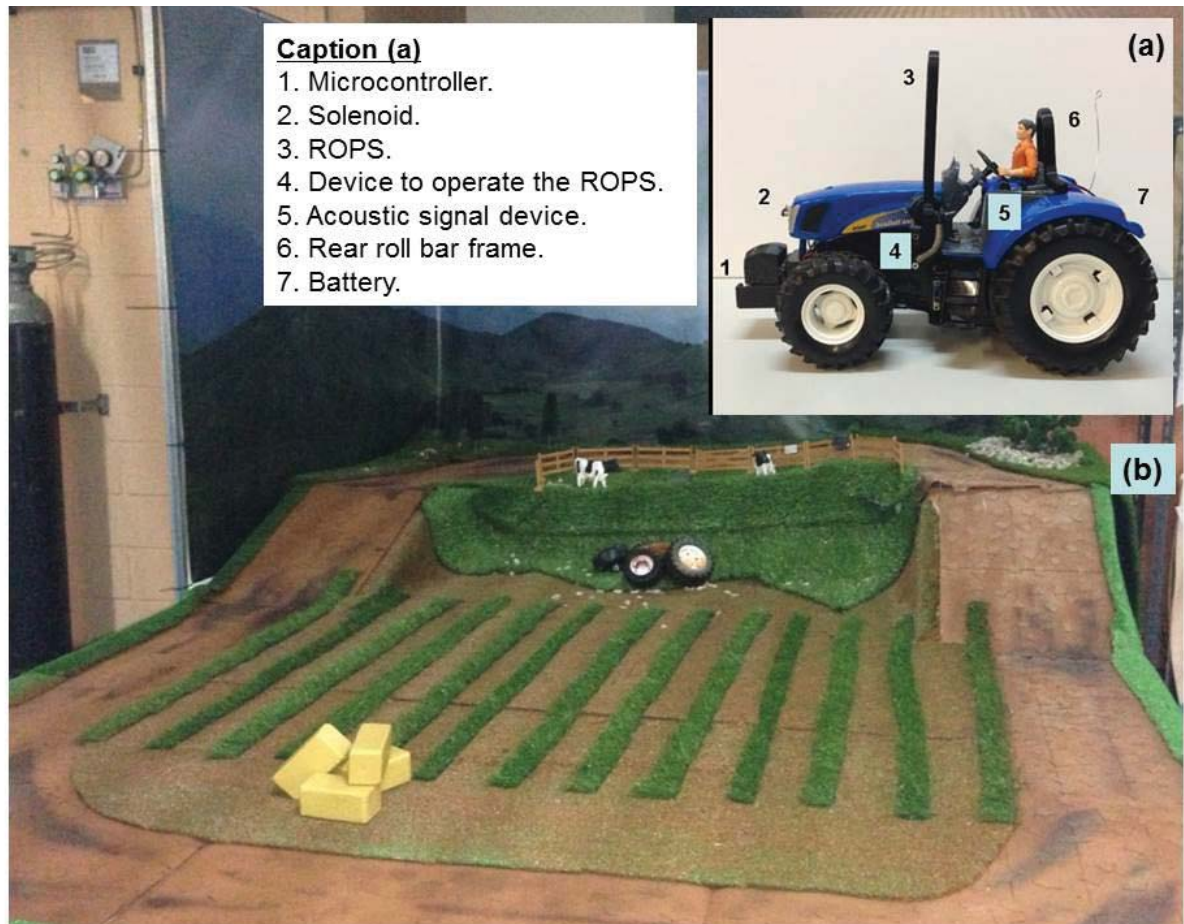


Figure 7. (a) scale tractor, (b) test platform.

Figure 8

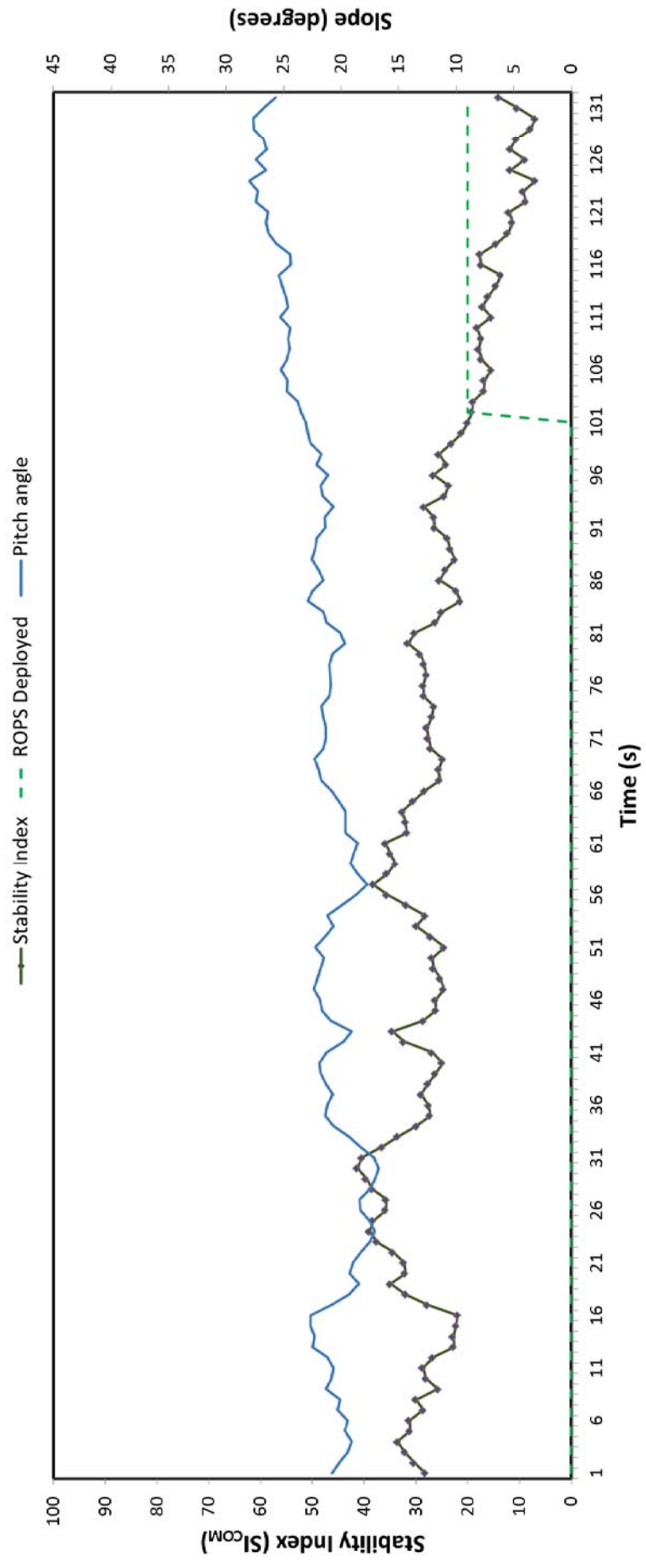


Figure 8. Pitch angle and stability index in a rearward upset field test.

Figure 9

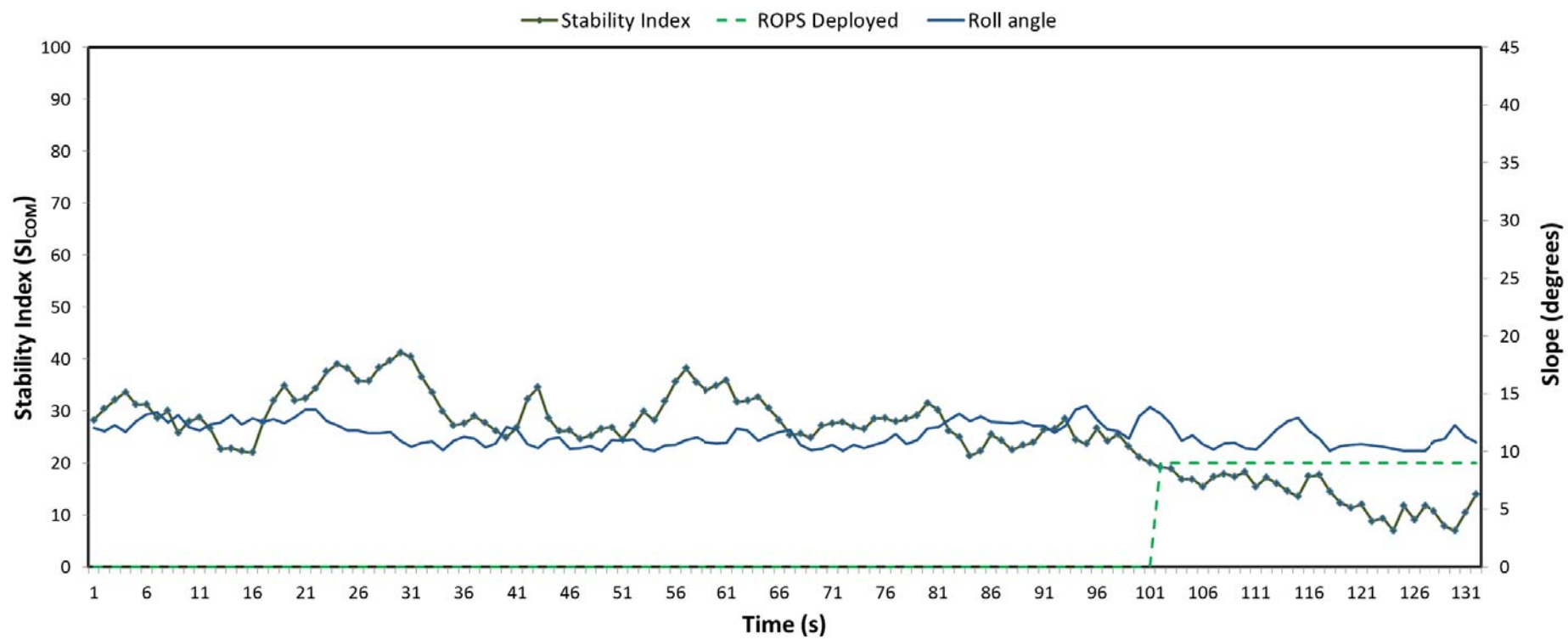


Figure 9. Roll angle and stability index in a sideward upset field test.