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Reducing-Effect of Chloride for the Dissolution of Black Copper

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Abstract: Oxidized black copper ores are known for their difficulty in dissolving their components of interest through conventional methods. This is due to its non-crystalline and amorphous structure. Among these minerals, copper pitch and copper wad are of great interest because of their considerable concentrations of copper and manganese. Currently, these minerals are not incorporated into the extraction circuits or left untreated, whether in stock, leach pads, or waste. For the recovery of its main elements of interest (Cu and Mn), it is necessary to use reducing agents that dissolve the present MnO₂, while allowing the recovery of Cu. In this research, the results for the dissolution of Mn and Cu from a black copper mineral are exposed, evaluating the reducing effect of NaCl for MnO₂ through pre-treatment of agglomerate and curing, and subsequently leaching in standard condition with the use of a reducing agent (Fe²⁺). High concentrations of chloride in the agglomerate process and prolonged curing times would favor the reduction of MnO₂, increasing the dissolution of Mn, while the addition of NaCl did not benefit Cu extractions. Under standard conditions, low Mn extractions were obtained, while in an acid-reducing medium, a significant dissolution of MnO₂ was achieved, which supports the removal of Cu.

Keywords: agglomerate; copper pitch; copper wad; curing; pre-treatment

1. Introduction

The interactions that occur in mineral deposits through geological agents help the formation of new mineral species [1]. An example is the oxidation of pyrite, which when reacted with water produces sulfuric acid, favouring the mobility of metals like copper, which under particular conditions of potential and pH can be transported, precipitating downstream, forming deposits called "exotic" [2]. The principal copper minerals being in this type of deposit are chrysocolla-atacamite, copper-pitch, and copper-wad [3].

The "copper wad" and "copper pitch" are hydrated silicates of manganese and iron, rich in copper, which appear as brotoidal masses, compact or earthy. When it is alone and shows earthy

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habit, it is called wad; if it is associated with chrysocolla, it is called pitch or "black chrysocolla" [4]. Pincheira et al. [5] proposed the name of black copper silicate to designate both mineraloids, without crystalline structure. They have a similar composition and in greater quantity are elements such as Cu, Mn, Fe, Al, and Si, accompanied by traces of Ca, Na, K, Mg, S, P, Cl, Mo, Co, Ni, As, Zn, Pb, U, V.

Black copper ores are a resource that is generally not incorporated into the extraction circuits or left untreated, whether in stock, leach pads, or waste [6,7]. This is due to the difficulty of recovering elements of interest like Cu or Mn by conventional hydrometallurgical processes since the complex structure is non-crystalline or amorphous [8]. However, several studies have been carried out to extract these elements from marine nodules and other manganese minerals, which generates alternatives for processing by similar leaching systems.

Several studies have been carried out in recent years for the extraction of Mn from marine nodules in acidic media, testing diverse reducing agents such as oxalic acid [9], glucose [10], FeO [11], cane molasses [12], corn cob [13], biomass from residual tea [14], etc. Toro et al. [15,16] obtained promising results when employing $FeSO_4$, formed from the reaction between tailings and H_2SO_4 . Benavente et al. [7] conducted a study for the dissolution of Cu and Mn from black copper under oxidizing and reducing conditions. The authors indicated that at oxidizing conditions, better results are not obtained than in a standard state (without oxidizing agents or reducing agents), concluding that the addition of an oxidizing agent does not improve the dissolution rate of black copper. Otherwise, in a reducing condition, the decrease in redox potential favors the dissolution of manganese, increasing the extraction of Cu.

Wang and Zhou [17] investigated the recovery of cobalt from residues of zinc plants by a hydrometallurgical process, using ammonium peroxydisulfate ((NH₄)₂S₂O₈) for the precipitation of manganese as MnO₂. The researchers noted that the chloride ion negatively affected manganese precipitation, which was attributed to the reduction of manganese oxide. The standard redox potentials are: Mn₃O₄/Mn²⁺ = 1.76 V and Cl₂/Cl⁻ = 1.39 V. Then, it was concluded that manganese oxide could be thermodynamically reduced to Mn²⁺ through chloride. Fuerstenau and Han [18] indicated that by working at 100 °C in the leaching of marine nodules, good extractions of copper, nickel, and cobalt could be obtained after a long period of residence, either with sulfuric acid or hydrochloric acid. Senanayake [19] compared the leaching of marine nodules in H₂SO₄ and HCl, in temperature ranges of 30–90 °C, with absence and presence of SO₂, Na₂SO₃, NaCl, and CaCl₂, concluding that at a higher temperature (90 °C) the HCl gives better results.

For the dissolution of manganese from black copper with the use of sulfuric acid and chloride, the following series of reactions is proposed:

$$(CuO \times MnO_2 \times 7H_2O)_{(s)} + 3H_2SO_{4(aq)} + 2FeSO_{4(aq)} + 2NaCl_{(s)} = Fe_2(SO_4)_{3(aq)} + MnCl_{2(aq)} + CuSO_{4(aq)} + Na_2SO_{4(aq)} + 10H_2O_{(l)} \tag{1}$$

$$MnO_{2(s)} + 2Fe^{2+}_{(aq)} + 4H^{+}_{(aq)} = Mn^{2+}_{(aq)} + 2Fe^{3+}_{(aq)} + 2H_2O_{(l)} \Delta G^0 = -88.5 \text{ kJ}$$
 (2)

$$2FeSO_{4(aq)} + 2H_2SO_{4(aq)} + MnO_{2(s)} = Fe_2(SO_4)_{3(s)} + 2H_2O_{(l)} + MnSO_{4(aq)} \Delta G^0 = -200 \text{ kJ}$$
 (3)

$$4NaCl_{(s)} + 2H_2SO_{4(aq)} + MnO_{2(s)} = 2Na_2SO_{4(aq)} + MnCl_{2(aq)} + Cl_{2(g)} + 2H_2O_{(l)} \Delta G^0 = -73.5 \text{ kJ}$$
 (4)

On the other hand, pre-treatment processes that involve agglomeration and curing stages have shown positive results to improve mineral reaction rates [20,21]. In the study conducted by Bahamonde et al. [22], pre-treatment with sodium chloride and sulfuric acid was carried out to enhance copper extractions in a concentrate formed mainly by bornite and chalcopyrite. Different concentrations of sodium chloride (15, 30 and 60 kg/t) and cure time (15 and 30 d) were studied, where finally, a significant increase in Cu extractions was obtained. In a more recent study by Cerda et al. [21], pre-treatment experiments were carried out for a copper sulphide mineral (chalcopyrite), where sulfuric acid (20 kg/t) and sodium chloride were added at different concentrations (20, 50, and 90 kg/t). The authors concluded that the cure time is more important than the level of chloride in the agglomerate process.

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Currently, the mining industry must generate a new approach that helps overcome the stagnation in its growth. Despite its surplus-generating role, large-scale mining faces significant challenges such as the deterioration of the ore grade, increased operational costs, and input costs must be adjusted to the demand for sustainable development [23]. In recent years, in Chile the treatment of other commodities has been incorporated into the extraction processes, for example, the recovery of Mo together with the Cu in flotation processes has been encouraged [24]. This helps to diversify the business and boost the export of additional products [6]. It is necessary to incorporate the minerals of black copper in the leaching processes, because of their considerable amounts of Mn (29%) which, when dissolved, favor the extraction of Cu, and would allow giving a high commercial value of these "residues".

In this research, the outcomes for the dissolution of Mn and Cu from a black copper ore are exposed. The reducing effect of NaCl for MnO_2 was evaluated by pre-treatment, adding this reagent in the agglomerate stage and then leaving it at rest. Subsequently, a leaching process was carried out under standard conditions and adding a reducing agent (Fe²⁺).

2. Experimental

2.1. Black Copper Simple

For the present study, a sample of black copper from a mining company in northern Chile was used. The sample was from a high-grade vein, with purity near to 100%. The ore was ground in a porcelain mortar to sizing between -173 and +147 μm. The chemical composition was determined by inductively coupled plasma atomic emission spectrometry (ICP-AES) (see Table 1). A QEMSCAN (Quantitative Evaluation of Minerals by SCANning) analysis was applied, which is a modified electronic scanning microscope, both in hardware and software. This performs the identification and automated quantification of ranges of elementary definitions that can be associated with inorganic solid phases (minerals, alloys, slags, etc.). The samples were mounted on briquettes and polished to determine the mineralogical composition. The identification, mapping of 2-D distribution, and quantification of inorganic phases were done by combining the emissions of retro-dispersed electrons (BSE), with a Zeiss EVO series, a Bruker AXS XFlash 4010 detector (Bruker, Billerica, MA, USA), and the iDiscover 5.3.2.501 software (FEI Company, Brisbane, Australia). The QEMSCAN analyses are based on the automated obtaining of EDS spectra (dispersed energy from X-rays), in hundreds of thousands or millions of collected analysis points, each in a time of milliseconds. The classification of mineralogical phases was done by classifying each EDS spectrum in a hierarchical and descending compositional list, known as the "SIP List". The BSE image was used to discriminate between resin and graphite in the sample, to specify entries in the SIP list, and to establish thresholds for acceptance or rejection of particles. As a result, pixelated, 2-D and false color images of a specimen or a representative subsample of particles are obtained. Each pixel retains its elementary and BSE brightness information, which allows subsequent offline data processing. Through software, customized filters are generated that quantify the ore and gangue species, mineral release, associations between inorganic phases, classifying particles according to criteria of shape, size, texture, etc. Figure 1 shows the chemical species to black oxides using QEMSCAN.

Table 1. Chemical composition of black oxide samples.

Mn (%)	Cu (%)	Fe (%)
22.01	40.24	7.92

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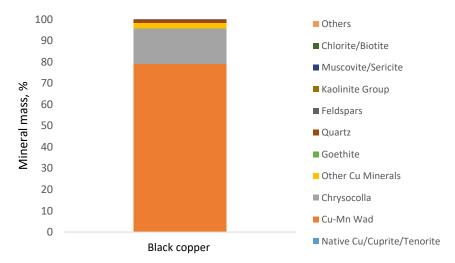


Figure 1. Detailed modal mineralogy.

Table 2 shows the mineralogical composition of the black copper samples. Copper wad refers to a subgroup of copper composed of manganese and copper hydroxides, as well as also traces of other elements such as Co, Ca, Fe, Al, Si, and Mg.

Table 2. The mineralogical	composition of the black co	opper samples as	determined by QEMSCAN.

Mineral (% Mass)	Black Copper
Native Cu/Cuprite/Tenorite	0.12
Cu-Mn Wad	78.90
Chrysocolla	16.72
Other Ču Minerals	2.69
Goethite	0.01
Quartz	1.41
Feldspars	0.02
Kaolinite Group	0.01
Muscovite/Sericite	0.01
Chlorite/Biotite	0.01
Others	0.09
Total	100

2.2. Ferrous Ions

The ferrous ions used for this investigation (FeSO₄ \times 7H₂O) were WINKLER brand, with a molecular weight of 278.01 g/mol. These were incorporated during the leaching process in stirred reactors, after the pretreatment process.

2.3. Pre-Treatment and Subsequent Leaching in reactors

For the pre-treatment, we worked with 10 g of ore, adding 20 kg of H_2SO_4/t (according to the level to be studied) and different concentrations of NaCl (See Table 1). The sample and reagents were homogenized and subsequently placed on a Petri dish, which was covered with plastic to avoid evaporation. The temperature during the resting time was controlled at 25 °C with the use of an air conditioner. Subsequently, leaching tests were carried out in a 100-mL glass reactor with a 0.01 S/L ratio. A total of 10 g of black copper ore and MnO_2 (manganese nodules) at different concentrations were mixed and dispersed with a five-position magnetic stirrer (IKA ROS, CEP 13087-534, Campinas, Brazil) at a speed of 600 rpm. The temperature was controlled at 25 °C using an oil-heated circulator (Julabo) (Julabo, St. Louis, MO, USA). All the tests were duplicated, and the measurements (or analyses) were carried out on 5 mL undiluted samples using atomic absorption spectrometry with a coefficient of variation \leq 5% and a relative error between 5 to 10%. Measurements of pH and oxidation-reduction

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potential (ORP) of leach solutions were made using a pH-ORP meter (HANNA HI-4222) (HANNA instruments, Woonsocket, RI, USA). The ORP solution was measured in a combination ORP electrode cell of a platinum working electrode and a saturated Ag/AgCl reference electrode.

2.4. Dissolution of Mn and Cu

In a previous research conducted by Wang and Zhou [17], it was discovered that after a long contact time, chloride could reduce MnO_2 . For this reason, it was resolved to assess this impact by agglomerate assays and subsequently a leaching process.

For the agglomerate tests, we worked by adding 20 kg of H_2SO_4/t and 10 kg of NaCl/t, with a curing time of 48 h. While the following operational parameters were used for leaching: Fe^{2+}/MnO_2 ratio of 1/1, particle size of -75 + 53 µm, agitation rate of 600 rpm, 1 mol/L sulfuric acid, and room temperature (25 °C).

2.5. Effect of NaCl Concentration and Cure Time

For the agglomerate and curing tests, we worked under the parameters presented in Table 3:

Test	Curing Time (h)	NaCl Concentration (kg/t)
1	48	10
2	48	20
3	96	10
4	96	20

Table 3. Variables studied in the pretreatment step.

For the leaching tests, the following operational parameters were worked: Fe²⁺/MnO₂ ratio of 1/1, particle size of $-75 + 53 \mu m$, agitation rate of 600 rpm, 1 mol/L sulfuric acid, and room temperature (25 °C).

3. Results

3.1. Effect of Agglomerate with NaCl to Dissolve Mn

Figure 2 shows the dissolution of Mn from a sample of black copper under four conditions: (1) without the use of reducing agent or prior agglomerate (standard state), (2) with the use of reducing agent (Fe^{2+}) without prior agglomerate, (3) without reducing agent, but with a previous agglomerate process (Standard condition + NaCl), (4) with previous agglomerate and use of reducing agent (Fe^{2+} + NaCl). It can be seen that without the use of a reducing agent, it is not possible to dissolve the Mn present in the black copper sample and, besides, a beneficial effect cannot be appreciated by adding chloride to the system. This is consistent with the results obtained by Benavente et al. [7], where Mn was not dissolved for a black copper ore under standard conditions. On the other hand, it can be seen that with the use of Fe^{2+} high solutions of Mn (over 50%) are obtained in short periods (20 min), a result very similar to that set forth by Pérez et al. [6] under similar conditions. When a previous agglomerate process is added by adding NaCl, a positive effect on the dissolution of Mn is generated. This allows confirming the statements made by Wang and Zhou [17], who indicate that the chloride being in contact with MnO₂ for a long time can generate a reducing effect on the mineral, favoring its subsequent leaching.

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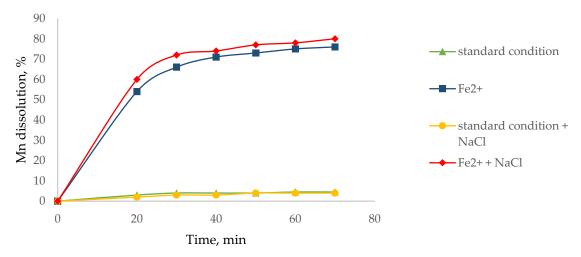


Figure 2. Dissolution of Mn from a black copper ore.

3.2. Effect of Agglomerate with NaCl to Dissolve Cu

Figure 3 shows the dissolution of Cu from a sample of black copper under the same conditions previously set out in Figure 2. There was no beneficial effect on the dissolution of copper when performing a previous agglomerate process by adding NaCl, but promising outcomes were achieved when adding a reducing agent. In the study conducted by Benavente et al. [7], it was indicated that no favorable results are obtained by adding O_2 for the dissolution of Cu from black copper ore. This situation was improved by working in a reducing condition, which favors the dissolution of MnO₂ by means of a reducing agent in an acid medium [11,25–27], allowing subsequent increase in Cu extractions.

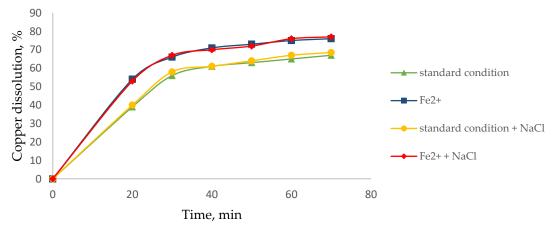


Figure 3. Dissolution of Cu from a black copper ore. Effect of NaCl concentration and cure time.

3.3. Effect of NaCl Concentration and Cure Time

Figure 4 shows the effect of carrying out a pre-treatment process by adding NaCl, giving a rest time and subsequently leaching the material. Sodium chloride did not generate any increase in the dissolution of Cu from black copper. However, a positive effect on manganese dissolution was seen, as the concentration of NaCl in the pre-treatment increased. In general, better results were obtained for both elements as the curing time increased, which is consistent with previous researches for the dissolution of Cu minerals [20,21]. A beneficial effect is also observed in the reductive leaching of MnO_2 over time, as the chloride concentration increased. The potential and pH values were in the range of -0.2 to 1.5 V and -0.5 to 0.4, for all the tests performed. These results are consistent according to the statement by Senanayake et al. [19], where it is indicated that the ranges of pH and potential suitable for a leaching of MnO_2 reductive using Fe are from -2 to 0.1 and -0.4 to 1.4 [28].

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In addition, when working in these ranges, Mn ions remain in solution, and do not precipitate through oxidation-reduction reactions [29].

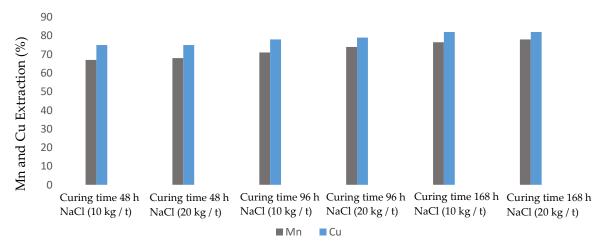


Figure 4. Effect of NaCl concentration and cure time on the dissolution of Mn and Cu.

Figure 5 shows that the main compound in the residues is copper oxide that has not yet dissolved, this oxide is from black copper, chrysocolla, and other copper oxides (tenorite, cuprite, among others) that were present in the initial mineral. The presence of copper-chloride complexes within the system stands out, this is mainly due to the curing with NaCl and the formation of solid species such as CuCl. The other species are oxides of manganese, iron and aluminum and silicon species, the latter elements originating from the chrysocolla and are present in small quantities in the mineral residue.

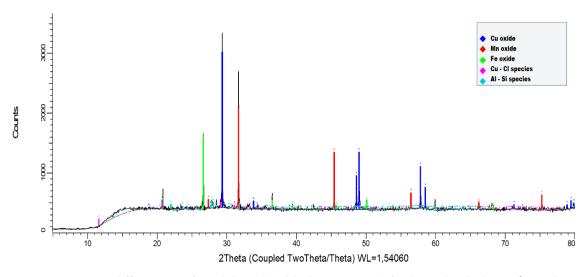


Figure 5. X-ray diffractogram for solid residue (black copper ore) after being leached at 25 $^{\circ}$ C with NaCl and FeSO₄ in a time of 70 min.

4. Conclusions

The present research displays outcomes where it is sought to dissolve Cu and Mn from black copper, with a pre-treatment of agglomerate incorporating NaCl, a cured time and subsequent acid-reducing leaching at room temperature (25 °C). The main findings are the following:

Under standard conditions, low Mn solutions were obtained, and pre-treatment with NaCl did not influence the solutions thereof.

When working in an acid-reducing medium, a more significant dissolution of MnO₂ was achieved, which favors the extraction of Cu.

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High concentrations of chloride in the agglomerate process and prolonged curing times would favor the reduction of MnO₂, increasing the dissolution of Mn.

An increase in curing time favors Cu solutions while the addition of NaCl in the agglomerate process is irrelevant for its dissolution.

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Conflicts of Interest: The authors declare they have no conflict of interest.

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